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## **INVENT SPECIFICATION**

Complete Specification Lodged ..... 3rd April, 1956.

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Applicant.....The Goodyear Tire & Rubber Company.

Actual Inventors.....Herbert Arthur Endres and Walter F. Winters.

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No drawing.

**COMPLETE SPECIFICATION.**

### **"RUBBERISED TAR COMPOSITION."**

The following statement is a full description of this invention, including the best method of performing it known to us:-

This invention relates to a tar composition having rubber-like properties and is more particularly directed to a material comprising a rubberized mineral carrier combined with tar and to a process for preparing the composition as well as uses thereof.

In the building of roads, asphalt is much used as a surfacing material but surfaces so prepared are not suitable for installations where solvents are constantly being spilled upon the surface. This difficulty has been brought to the fore by the necessity of providing suitable runways for jet aircraft, the jet fuel being subject to frequent spillage and being of a high boiling character and thus slow to evaporate. Thus, jet runways are subject to more or less constant attack by the solvent power of the jet fuels spilled upon them. For such uses, therefore, asphalt pavings are not suitable since the asphalt is soluble in the jet fuel and the runway quickly deteriorates.

It has now been discovered that tar, when suitably treated, provides an excellent surfacing material for jet runways. This is true even though tars are normally much softer than asphalts. The runway surface is prepared by adding to a tar a small amount of rubber, the tar thus treated becoming stabilized against changes in its physical properties due to temperature variations but, most importantly, offering great resistance to solvent attack by the jet fuels. The rubber must be incorporated in powder form, as will be set forth hereinafter, and best results are obtained if the rubber is of an oil-resistant type, specifically, a butadiene-acrylonitrile copolymer. In order to obtain readily dispersible unvulcanized rubber in powder form a mineral carrier is co-precipitated with latex rubber. This invention is concerned with a process for incorporating rubber in tar rapidly and in such a manner as to obtain the maximum benefits from the rubber.

It is, therefore, an object of this invention to provide a rubberized tar composition. It is another object of this invention to provide a composition of rubber and mineral filler which can be quickly incorporated into tars. It is a further object of this invention to provide a rubberized barytes powder which can be rapidly dispersed in hot tars. It is still another object of this invention to provide a rubberized barytes powder which can be rapidly dispersed in a mixture of hot tars and aggregates to form a surfacing composition. Other objects will be apparent as the description proceeds.

In the practice of this invention a rubber powder is first prepared by mixing a water suspension of a mineral filler or carrier with a rubber latex and then co-precipitating by means of a coagulant. The coagulated compound is filtered from the slurry, dried and pulverized. The product is inexpensive, easy to handle because it is free-flowing, and readily dispersible in tars.

A preferred inert carrier which is especially adapted to the practice of this invention is a finely divided pulverulent barytes mineral such that all particles will pass a 200-mesh standard sieve and such that substantially all particles pass a 325-mesh standard sieve. A particularly suitable mineral is the mineral content of the effluent from barite ore refining wherein 90% of the barytes mineral particles are finer than 10 microns in diameter and 50% of them have a particle size of less than 5 microns. This barytes mineral composition may be composed of from about 50% to about 90% by weight of barium sulphate together with natural impurities such as quartz and compounds of silica. This composition is particularly adapted to the practice of this invention because it has the inherent properties of high specific gravity coupled with relative softness and it has an affinity for tars which helps carry the rubber

component rapidly into complete amalgamation with the tar. Although barytes is preferred in the practice of this invention, other non-fully equivalent inert minerals display many of the advantages imparted by barytes and may be used in the practice of the invention. For example, finely ground minerals such as perlite, fly-ash, ground quartz, clay, diatomaceous earth, soapstone, bentonite, ground limestone, and perversulent carbon, ranging in size from 1 to 40 microns, can be used as carriers.

The barytes mineral, in an amount of about 5 to 30 parts by weight, can be slurried with about 95 to 70 parts by weight of water. The pH of the slurry is adjusted to about 8.0 to 9.5 to prevent premature coagulation of the rubber. To this slurry about 2 to 12 parts by weight of 30% nitrile rubber latex is added or an equivalent amount of rubber solids from various other oil-resistant latices of various rubber concentrations may be used. The slurry of rubber latex and carrier is agitated until a homogeneous mixture is obtained.

While it has been found that many types of unvulcanized latex rubber may be used in the practice of this invention, such as natural rubber latices, polyisobutylene latices, polychloroprene latices, butadiene-styrene latices, i.e., GR-S latices, polybutadiene latices, acrylonitrile latices, i.e., butadiene-acrylonitrile latices, isoprene-acrylonitrile latices or ethyl acrylate-acrylonitrile latices, polyisoprene latices and polysulfide latices, it is preferred to use butadiene-acrylonitrile latices, especially those wherein the ratio of butadiene and acrylonitrile ranges from about 50 to 85% of butadiene by weight to 15 to 50% of acrylonitrile by weight. These nitrile rubbers are preferred since, with these, maximum resistance to solvent attack is achieved.

After the latex-filler slurry has been thoroughly mixed, a coagulant is added to precipitate the solids from the mixture. Any of the customary coagulants can be used. Representative coagulants are aluminum sulphate, sodium chloride, barium chloride, calcium chloride, magnesium sulphate, hydrochloric acid and sulphuric acid.

Although the particle size of the composition can be varied within limits it is preferred to coagulate the rubber and mineral as particles of about 50 to 200 microns in diameter. The rubberized mineral particles will normally pass through a 60-mesh standard screen. The resulting rubber-filler particles can be subsequently de-watered, dried and pulverized to break up aggregates to form a fine free-flowing power for ready use in tar applications.

The final rubber-mineral filler product may contain from about 10 to 40 percent by weight of rubber and from about 90 to 60

percent by weight of filler. In the practice of this invention we have found that a dry pulverized composition containing 25.0% by weight of nitrile rubber and 75.0% by weight of filler gives very satisfactory results. At least 85% of this composition should pass through an 80-mesh standard sieve and about 55% should pass through a 200-mesh standard sieve. Another rubber-mineral filler composition used in carrying out the invention is ore in which a rubbery-copolymer of butadiene and acrylonitrile is present in a relationship of about 10 to 60% by weight to about 90 to 40% by weight of filler.

The rubber-mineral carrier composition remains remarkably free-flowing and storage-stable. This is believed to be due to the manner of distribution of the barytes and rubber in the powder, the dry composite apparently consisting of groups of barytes particles having interlaced therewith and spread over and interlocked with their irregular surface areas thin films of unvulcanized rubber in a discontinuous phase, particles of barytes protruding through the rubber films to act as non-tacky contacting surfaces. This composite rubber-barytes particle material is and remains in the form of a loose, free-flowing powder which can be rapidly dispersed in tars.

The dry rubber-mineral filler composition can be mixed with tar in an amount large enough to add sufficient rubber to impart satisfactory stabilization but small enough to keep from deleteriously affecting the properties of the tar by increasing the viscosity too much. In order to provide satisfactory results, the rubber content should be at least 0.5% by weight and not over 15.0% by weight, based on the weight of tar, 1.0% to 5.0% being preferred. The amount of dry rubber-mineral filler added will obviously vary with the composition of the filler. When the filler is comprised of the preferred 25 to 30% by weight of rubber to 75 to 70% by weight of mineral carrier, about 5% by weight to about 40% by weight of dry rubber-mineral carrier filler can be mixed with about 95% by weight to about 60% by weight of tar to impart the desired characteristics without deleteriously affecting the tar by increasing the viscosity too much.

The powdered rubberized mineral can be quickly and conveniently hot-mixed with tar and aggregate in an ordinary pug mill which is conventionally used in paving operations to form a paving mixture. Also, if desired, the rubberized carrier can be premixed with one or more of the herein-described tars and thereafter combined with ordinary aggregate to form a paving mixture.

The tars, which term is used herein to include also pitches derived from the respective tars, which are useful in the practice of this

invention are viscous to hard compositions which may be referred to as pitchy tars, resulting from the destructive distillation of carbonaceous materials, and characterized by having a water-insoluble residue upon sulfonation of from 0% to 40% by original weight of the carbon disulfide-soluble portion of the tar, in accordance with the test set forth on pages 1213-1214 of the book by Herbert Abraham entitled "Asphalts and Allied Substances", Fifth Edition, Van Nostrand, New York, 1945. In accordance with this test, three grams of the carbon disulfide-soluble portion of the substance are mixed with 6 cc of concentrated sulfuric acid in a test tube and agitated for a period of 45 minutes with the test tube surrounded with boiling water. The contents of the test tube are then poured into 500 cc of cold water, and after a period of two hours standing, the precipitate, if any, is decanted, filtered, washed, dried, and weighed.

The tars and pitches of this invention are further characterized by giving a positive diazo reaction when tested according to the diazo reaction described in detail on pages 1234 and 1235 of the Abraham reference, cited above. Reference is made to the Abraham work cited for further details.

Depending on the source, the various tars are referred to as oil gas tars, water gas tars, pine tars, hardwood tars, peat tars, lignite tars, shale tars, coal tars, and bone tars. The various coal tars, which are preferred in the practice of this invention, are further referred to as coke oven tars, vertical retort tars, horizontal retort tars, and low temperature tars.

The useful tars for the practice of this invention are tars which have a softening point within the range of 25°C. to 70°C., particularly tars having a softening point within the range of 40°C. to 70°C. Preferred tars are pitchy coal tars identified as RT tars by the U. S. Government Federal Standard Stock Catalog issued by the Bureau of Public Roads. These tars, which have been given numerical identifications of RT-1 to RT-12, RTCB-5 and RTCB-6, are further defined in Highway Materials, 8th ed., Part 1, pages 31 and 32, published by the American Association of State Highway Officials, 1955. The RT-7 to RT-12 tars are particularly useful in practicing this invention, RT-12 being preferred. This coal tar has a specific gravity at 25°C. of 1.16, 75% by weight of total bitumen, less than 10% of distillable content at 270°C., less than 20% distillable content at 300°C., and a softening point of 40°C. to 70°C.

In the practice of this invention it is essential that the rubberized mineral filler be substantially anhydrous and that the pitchy tar also be substantially free of moisture. If the rubberized carrier contains

moisture the desirable factors of storage stability, free flowability and rapid dispersion are adversely affected. Any substantial amount of moisture must be evaporated during the mixing cycle before the composition can be laid on the base to be surfaced. Because the mixing time is as short as one-half to one and one-half minutes, no time can be allowed for evaporation of moisture. Even if the mixing cycle would permit evaporation, moisture deleteriously affects the rapid dispersion which is essential in obtaining the complete amalgamation which is necessary if the small amount of rubber is to display the maximum effectiveness. Thus, the rubberized fillers and the pitchy tars must both be substantially anhydrous.

The invention is more clearly understood when described in connection with a particular preferred tar, RT-12 coal tar, which has been rubberized with a substantially anhydrous rubber-mineral carrier filler, although it is to be understood that the invention is not limited to a particular tar. When a powdered mixture containing 30% nitrile rubber and 70% barytes was added to RT-12 coal tar in the proportion of 3% rubber, based on the weight of the tar, the softening point of the tar was raised from approximately 95°F. (35°C.) to 115°F. 46.1°C, Brookfield viscosities were raised from 600 at 200°F. (93.3°C.) to 2,000 at 200°F. (93.3°C.), penetrations at 77°F. (25°C.) were lowered from a very soft 250 which was difficult to measure down to about 150. The tar-rubber materials had improved high temperature stability and increased low temperature flexibility. In addition, rubberizing the tar reduced oxidation and cracking as compared to the ordinary tar aggregate hot mixes. It was further noted that the tar became more dense and thus provided a more impermeable binder. This composition was used in a standard test developed by the Corps of Engineers whereby test panels were constructed and jet fuel was spilled onto the surface at a four-hour intervals for a period of six weeks. The rubberized RT-12 was far more resistant to penetration by the fuels than untreated RT-12 tar. The rubberized RT-12 coal tar was subjected to a further test by being immersed in an aliphatic jet fuel. After 18 hours immersion at 100°F. (37.7°C.) the weight had changed only 0.71% and the volume had changed only 0.44%. Thus, the addition of rubber in the form of a free-flowing rubber-mineral powder has been shown to greatly improve the properties of coal tar.

In the preferred practice of this invention a dry mineral aggregate is heated to a temperature between 200-300°F. (93.3-149°C.) in a pug mill and thereafter one or more of the herein-defined tars are mixed with the heated aggregate. To the mixing chamber containing the aggregate and tar, the rubberized carrier is added so that a complete and uniform blending is effected. The mineral aggregate is usually

present in the proportion of about 85 to 95 percent by weight of the entire mixture and the rubberized tar in the proportion of about 5 to 15 percent. Thus, the rubber component of the paving mixture may be as low as 0.15% and still be effective in producing the desired result and may be present in a proportion as large as 0.5 to 5.0 percent. The relationship of rubber to total paving mixture will obviously depend on the contemplated use and type of rubber. The complete mixing cycle can usually be completed in from 1/2 to 1-1/2 minutes, the amount of time customarily available for on-the-job preparation of commercial paving mixtures. Thus, a novel feature of this invention is that it enables conversion of a tarry paving composition into a rubberized tarry paving composition in a short period of time and with the same equipment as used in the production of regular hot type paving mixtures.

It has not been completely established why or how the small amount of rubber thus added so markedly changes the properties of the tars. However, from a rheological standpoint, rubber must be highly dispersed in tars in order to display the maximum effectiveness. It is believed that a highly dispersible rubber composition such as the free-flowing powder of this invention, proceeds to ultimate dispersion in tars in three stages:

- (1) Rapid dispersion of the discrete rubber particle into the mass of the tar;
- (2) The partial or complete breakdown of the rubber particle into molecular or near molecular size, accompanied by effective "solution" in the tar; and
- (3) A structural rearrangement occurring between the tar micelle and the rubber molecule to form essentially a new material.

If a rubber exists merely as sticky particles it is not capable of passing through phases 1 and 2, and does not impart the desired changes to the tar. Ordinary crumb rubbers do not rapidly disperse and do not go through phases 1 and 2, whereas the products of this invention become readily dispersed and exhibit the maximum effect in stabilizing the tars against deterioration from aliphatic fuels as well as against flow in hot weather and cracking in cold weather because of complete and rapid dispersion. Migration of the rubber in the tar probably continues for an appreciable period after the tar compositions are cast. Therefore it is highly important that the rubber particles be as completely dispersed as possible in order to provide the maximum number of rubber particles as centers of migration around which the tars are modified by the rubber migrating thereinto.

The compositions of this invention find greatest utility in

surfacing applications where fuels, particularly aliphatic fuels, are normally spilled. For example, jet aircraft operation results in considerable spillage of fuels before and during take-offs. Since this fuel is high-boiling, it does not evaporate quickly and remains on the runway to attack and deteriorate the surface thereof by dissolving constituents of such surfaces. Thus the invention is useful in the surfacing of jet airstrips.

Although the invention has been described with respect to jet airstrip surfacing compositions, it is to be understood that it can be used for any purpose where tars are normally used. Representative examples are service station aprons, seal coats for other materials, joint fillers, parking areas, streets, sidewalks, pit linings, facings for dikes around oil storage tanks, floorings (particularly industrial floors) revetments and jetties.

In the practice of this invention, the rubberized tar-aggregate hot mix is normally compacted to a thickness of about 1-1/2 to 2 inches on top of some form of base. The preferred base composition is a course of several inches of heavy aggregate topped by a customary asphalt surface. The rubberized tar-hot mix will bond with the asphalt so that the tar will not strip from the asphalt. All of the asphalt can be replaced by the rubberized tar mix of this invention if desired. Also, the rubberized tar mixtures of this invention can be layed as protective surfaces on existing pavements of various types such as bricks, concrete, asphalt and combinations thereof.

A further example of a preferred method of carrying out the invention comprising the steps of (1) laying about 6 to 12 inches of aggregate ranging in size from about 1 to 3 inches in diameter on a well-drained earthen base, (2) coating said aggregate with about 2 to 4 gallons of asphalt per square yard, and (3) topping said asphalt with from 1 to 3 inches of a rubberized pitchy tar hot mix which is prepared by mixing about 10% to 40% by weight of a petroleum-resistant unvulcanised nitrile rubber in latex form with about 90% to 60% by weight of barytes mineral in a slurry, coprecipitating and drying the nitrile rubber and barytes to form dry free-flowing particles capable of passing through a 60-mesh standard sieve, adding said dry powdered rubberized barytes to a pitchy tar having a softening point of about 25°C. to 70°C. in order to incorporate from 0.5% to 5.0% by weight of rubber into the pitchy tar, said aggregate being present in an amount of about 85% to 95% by weight.

While certain representative embodiments and details have been shown for the purpose of illustrating the invention, it will be apparent to those skilled in this art that various changes and modifications may be made therein without departing from the spirit or scope of the invention.

The claims defining the invention are as follows:-

1. A method of uniformly distributing an unvulcanized rubber in pitchy tar which comprises mixing said pitchy tar with a free-flowing rubber-containing powder which acts as a vehicle for incorporating said rubber in said pitchy tar, said free-flowing powder containing from 10% to 40% by weight of rubber and from 90% to 60% by weight of a mineral carrier and being capable of passing through a 60-mesh standard screen. (16th November, 1955)

2. A method of adding an unvulcanized rubber to pitchy tar which comprises mixing said pitchy tar with particles of a free-flowing rubber-containing powder, said particles ranging in size from about 100 to 200 microns and containing a mineral filler and a rubbery copolymer of butadiene and acrylonitrile said filler and copolymer of butadiene and acrylonitrile being present in a relationship of about 90% to 40% by weight of filler to about 10% to 60% by weight of copolymer of butadiene and acrylonitrile. (16th November, 1955)

3. A method of surfacing comprising preparing a composition of a pitchy coal tar and a free-flowing readily-dispersible powder capable of passing through a 60-mesh standard screen and comprising about 95% by weight to about 60% by weight of pitchy coal tar and about 5% by weight to about 40% by weight of a free-flowing readily-dispersible powder, said powder comprising about 10% by weight to about 40% by weight of an unvulcanized rubber and about 90% by weight to about 60% by weight of a finely divided mineral, mixing said composition of pitchy coal tar and free-flowing readily-dispersible powder with a mineral aggregate and spreading the resulting mixture on a base. (16th November, 1955)

4. A surface comprising a pitchy coal tar, aggregate, and a free-flowing rubber-mineral additive powder, said free-flowing rubber-mineral additive powder containing from 10% to 40% by weight of an unvulcanized rubber and from 90% to 60% by weight of a mineral filler, said free-flowing rubber-mineral additive powder being capable of passing through a 60-mesh standard screen and being present in said road surface in less quantity than said pitchy coal tar. (16th November, 1955)

5. A surface comprising a pitchy coal tar, aggregate, and a free-flowing rubber-mineral additive powder, said free-flowing

rubber-mineral additive powder containing from 10% to 40% by weight of a copolymer of butadiene and acrylonitrile wherein the butadiene content ranges from about 50% to 85% by weight and from 90% to 60% by weight of a mineral filler, said free-flowing rubber-mineral additive powder being capable of passing through a 60-mesh standard screen and being present in said road surface in less quantity than said pitchy coal tar. (16th November, 1955)

6. A method of preparing a substantially anhydrous pitchy coal tar surfacing composition comprising the steps of (1) preparing a substantially anhydrous storage-stable free-flowing powder, capable of passing through a 60-mesh standard screen and capable of dispersing readily in coal tar, from a mixture of an unvulcanized rubber and a mineral filler, said unvulcanized rubber being present in an amount of 10% to 40% by weight and the mineral filler being present in an amount of 90% to 60% by weight of the powder, and (2) mixing said storage-stable free-flowing finely divided powder with substantially anhydrous pitchy coal tar to form said pitchy coal tar surfacing composition. (16th November, 1955)

7. A method of preparing a substantially dry pitchy coal tar surfacing composition comprising the steps of preparing a substantially dry free-flowing powder capable of dispersing readily in coal tar and capable of passing through a 60-mesh standard screen containing from 10% to 40% by weight of unvulcanized rubber and from 90% to 60% by weight of a mineral filler, by the simultaneous coagulation of an unvulcanized rubber from a rubber latex and the removal of water from a water slurry of a mineral filler drying the same and mixing the said free-flowing powder with a coal tar which is substantially free of water. (16th November, 1955)

8. A method of preparing a substantially anhydrous pitchy coal tar surfacing composition comprising the steps of preparing a substantially dry readily-dispersible free-flowing powder by mixing about 10% to 40% by weight of unvulcanized nitrile rubber in latex form with about 90% to 60% by weight of mineral barytes in a water slurry, simultaneously coprecipitating the nitrile rubber and barytes mineral and drying the same so that the dry particles are capable of passing through a 60-mesh standard screen, heating about 85% to 95% by weight of aggregate with a substantially dry pitchy coal tar in a mill, adding the nitrile rubber-barytes powder to the mixture of hot tar and aggregate and thereafter mixing the same for a period of  $1\frac{1}{2}$  to  $1\frac{1}{2}$  minutes to form a

rubberized tar hot mix. (16th November, 1955)

9. A substantially dry surfacing composition comprising a mixture of aggregate, a pitchy coal tar having a softening point of about 25°C. to 70°C. and a rubberized barytes comprised of about 10% to 40% nitrile rubber and 90% to 60% by weight of barytes mineral, said rubberised barytes powder comprising about 5% to 15% by weight of the total mixture being capable of passing through a 60 mesh standard screen. (16th November, 1955)

10. The method of producing a rubber-containing pitchy tar composition suitable for use as a construction material which comprises incorporating a free-flowing powder capable of passing through a 60-mesh standard sieve comprised of petroleum-resistant unvulcanized rubber in the form of a composite with a finely divided character in the proportion of 10% to 40% by weight of rubber and 90% to 60% by weight of mineral carrier, with a pitchy tar having a softening point of about 25°C. to 70°C. (16th November, 1955)

11. The process of preparing a surface comprising the steps of (1) laying about 6 to 12 inches of aggregate ranging in size from about 1 to 3 inches in diameter on a well-drained earthen base, (2) coating said aggregate with about 2 to 4 gallons of asphalt per square yard, and (3) topping said asphalt with from 1 to 2 inches of a rubberized pitchy tar hot mix which is prepared by mixing about 10% to 40% by weight of a petroleum-resistant unvulcanized nitrile rubber in latex form with about 90% to 60% by weight of barytes mineral in a slurry, coprecipitating and drying the nitrile rubber and barytes to form dry free-flowing particles capable of passing through a 60-mesh standard sieve, adding said dry powdered rubberized barytes to a pitchy tar having a softening point of about 25°C. to 70°C. in order to incorporate from 0.5% to 5.0% by weight of rubber into the pitchy tar, said aggregate being present in an amount of about 85% to 95% by weight. (16th November, 1955)

12. The method of producing a substantially anhydrous rubber-containing pitchy tar composition suitable for use as a construction material which comprises mixing a dry free-flowing powder capable of passing through a 60-mesh standard sieve, said powder being comprised of an unvulcanized rubbery copolymer comprised of from 50% to 85% of butadiene and from 15% to 50% of acrylonitrile combined with finely divided mineral barytes in the production of about 10% to 40% by

weight of unvulcanized rubber and 90% to 60% by weight of mineral barytes with an RT pitchy tar having a softening point of about 40° C. to 70° C. (16th November, 1955)

13. A substantially anhydrous, rubber-tar composition comprised of a major amount by weight of pitchy coal tar having a softening point of from about 25° C. to 70° C., and a minor amount by weight of rubberized barytes powder comprised of from about 10% to about 40% nitrile rubber and from about 90% to about 60% by weight of barytes mineral. (16th November, 1955)

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Patent Attorneys for Applicant.

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References:-

<u>Serial No.</u>	<u>Application No.</u>	<u>Classification</u>
160,436	7777/52	47.5;47.7;81.7;18.7
165,932	27,091/54	18.7;47.7;79.3
165,931	27,090/54	18.7;47.7;79.3

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